



Stat Teaser

ABOUT STAT-EASE® SOFTWARE, TRAINING, AND CONSULTING FOR DOE • MARCH 1998
 Phone: 612-378-9449 • Toll-Free: 800-801-7191 • E-mail: info@statease.com • Website: www.statease.com

Workshop Schedule

• Experiment Design Made Easy

April 14–17, 1998: Minneapolis, MN

May 5–8, 1998: Dallas, TX

June 2–5, 1998: Minneapolis, MN

Covers the practical aspects of Design of Experiments (DOE). Learn about simple but very powerful two-level factorial designs.

• Response Surface Methods for Process Optimization

June 23–26, 1998: Minneapolis, MN

October 6–9, 1998: Minneapolis, MN

This workshop builds factorial DOEs into Response Surface Methods (RSM), which produce maps to help find the optimum and/or robust conditions for your process.

• Mixture Design for Optimal Formulations

March 17–20, 1998: Minneapolis, MN

July 14–17, 1998: Minneapolis, MN

If you do product formulation, you know that standard factorial designs just don't work. You need the mixture design skills presented here.

• Robust Design for Quality Improvement

April 28–30, 1998: Minneapolis, MN

December 7–9, 1998: Anaheim, CA

Learn to meet your tightest specifications with minimal variation. Push the envelope with saturated fractional factorials.

• Real Life DOE (see page 2)

May 12–14, 1998: Minneapolis, MN

Sept. 29–Oct. 1, 1998: Minneapolis, MN

Learn the tricks to analyzing real life DOEs!

Attendance limited to 24. Reserve your place by calling Carol, ext. 18, at

800-801-7191

Or, bring us on site. Ask for a quote.

Bad Leverages?

Question: Why do some of my leverages get flagged as “bad” after reducing my model?

Pat's Stat Tips

Answer: They may get flagged, but they're not bad!

Leverage is the amount of potential each design point exerts based on its position in the design space and the model being fit. The maximum leverage any point can have is 1. (The maximum leverage a replicated point can have is one divided by the number of replicates.) To illustrate, let's look at a linear model fit to two unique design points, one of which is replicated.

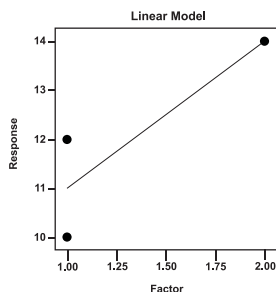


Figure 1: Plot of Linear Model

The two replicates of factor level 1 each have a leverage of 0.5 and the model fits their average. The single replicate of factor level 2 has a leverage of 1.0 and is fit perfectly. A leverage of one implies a point must be fit perfectly by the model and any error associated with the point is built into the model. For this reason, high leverage points are not desirable. In the case statistics section of the ANOVA report, Design-Ease® and Design-Expert® software “flag” points with leverages greater than two times the average leverage. But if leverages get flagged after model reduction,

don't be overly concerned.

Let's illustrate the principles of leverage using a two-factor, face-centered Central Composite Design (CCD). This is a response surface design composed of 1) factorial points — located at the corners of the square to give information about linear and interaction coefficients; 2) axial points (star points) — these give information about the pure quadratic and linear coefficients; and 3) center points (replicated) — these give information about the pure quadratic coefficients.

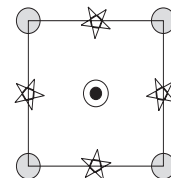


Figure 2: Face-Centered CCD

We'll analyze the response shown on table 3 and fit the full quadratic model. The statistical results are shown below:

Factor	Coefficient Estimate	t for H ₀ : Coeff=0	Prob> t
Intercept	99.31		
A-Factor A	-5.44	-14.65	<0.0001
B-Factor B	7.79	20.98	<0.0001
A ²	0.51	0.93	0.3810
B ²	0.49	0.89	0.4034
AB	-11.37	-25.01	<0.0001

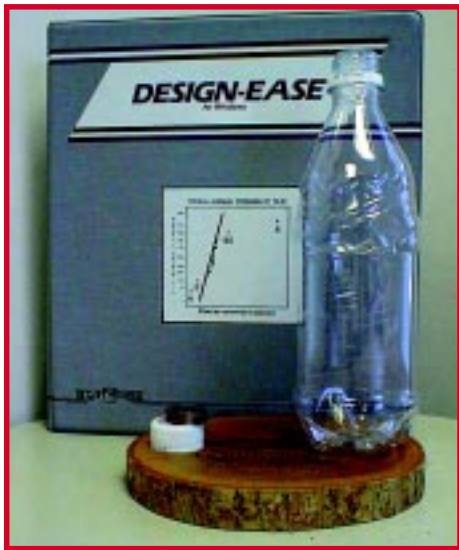
Table 1: Full Quadratic Model

— continued on page 4

Mysterious March of the Sugar-Pop Soldiers

"It's eerie," my colleague John Guerin said when I demonstrated how long a plastic pop bottle will wobble when placed upon certain surfaces. While John taught his portion of a class on DOE, I was experimenting in the back with an empty root-beer bottle, killing time — at 25 seconds a wobble to be precise. (Engineers are easily amused!)

You've no doubt drunk from one of these bottles. They've got an unusual star-shaped bottom with five blunt



points. I can't explain why they're shaped so strangely, but I can tell you that

Mark's Experiment

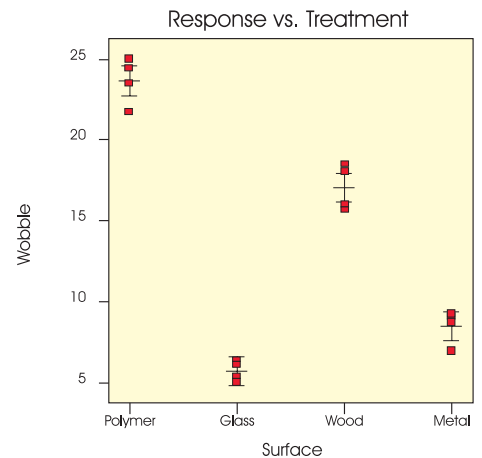
by Mark J. Anderson

they're very unstable when emptied. This is not a trivial issue in the Anderson home because we've got tons of teenagers hanging around guzzling caffeinated colas. The empty bottles multiply in Tribble-like fashion. The vibrations from my son's multi-megawatt sub-woofer bring these "dead soldiers" back to life. They wobble drunkenly across the countertops and over the edge, dribbling their syrupy residual on the floor. Yuk!

After class I tried to reproduce the astounding wobble of the plastic pop bottle. I thought I might do a two-level DOE on various amounts of residual liquid, tip height, cap weight, and the like. However, no matter how hard I tried, I could not get the bottle to wobble more than five seconds. Then I realized that it was the surface that made the difference. I was doing the experiment on a glass coffee table, whereas the table in class was clad in a polymeric material. Sure enough, when I tipped the bottle on the similarly surfaced bathroom counter, I got the complete 25-second dance. This led me

to experiment on other surfaces: metal and wood.

The results from five trials each are shown on the effects graph from Design-Ease® software. Notice that the least significant difference (LSD) bars do not overlap. Therefore, it can be said with greater than 95 percent confidence that all sur-



faces differed. The order in decreasing effect is polymer > wood >> metal > glass.

Of course these surfaces were all unique in terms of smoothness, thickness, and other material properties. I have no idea why they should interact so differently with the bottle.

My data came from a 20-ounce PETE-plastic bottle tipped from an eight-millimeter height (the width of four quarters). Next time you're stuck in a boring meeting or delayed at the airport, check it out for yourself. In Minneapolis and several other terminals you can go to the Cheer's bar and order a bottle. For inspiration you can sit next to the life-size dummy of Cliff Clavin, the nerdy postman. Perhaps he'll explain the wobbling as follows: "This here is a phenomenon caused when the elastic moduli match, which creates a harmonic wave, dampened in various ways by ambient temperature and humidity, etc., etc., etc."

Any other theories?

— Mark Anderson (e-mail: mark@statease.com)

Real Life DOE Workshop!

Our newest class, designed by student request, teaches you how to deal with difficult data analysis decisions such as:

- What should you do when you have several outliers?
- How can proper residual analysis help you salvage data?
- How can my data be interpreted best? for specialized analysis.



All of these questions and more will be answered in our "Real Life DOE" workshop! The computer-intensive format leads you through the most interesting and informative cases from the extensive Stat-Ease files. Students are encouraged to bring their own data

Call Carol NOW to reserve your place
800-801-7191, ext. 18

Introducing the Stat-Ease Crew



Front Row (L to R): Brian Smith, Tryg Helseth, Carol Summer, Neal Vaughn, Jim Whitcomb. Back Row (L to R): Pat Whitcomb, Sherry Brostrom, Shari Kraber, Gina Herrman, Roxanne Murray, Tim Gogolin, Carl Polnaszek, Mark Anderson.

Stat-Ease Does Dallas!



Stat-Ease, Inc. will be visiting the great state of Texas several times this year!

On March 29, Mark Anderson has been invited to speak at the American Chemical Society National Conference (see the "Where Can You Find Us?" column). On May 5-8 we are conducting a public workshop, "Experiment

Design Made Easy," co-taught by Shari Kraber and Carl McAfee. If you want to sign up for this workshop, call Carol at 800-801-7191, ext. 18. On August 9-13 we will present two talks at the Joint Statistical Meetings hosted by the American Statistical Association.

If you would like more information about any of these activities, please call us or send e-mail to info@statease.com.

Reader Response to Mark's Shade Experiment

In the December 1997 issue of the Stat-Teaser, Mark reported that a shiny exterior was best for deflecting the bright sun. Now, a reader tells us why.

People who make and use telescopes try to keep their equipment from cooling down too much under clear cold night skies. (When it is too cold, dew forms.) The basic physics are similar to the hot or cold car problem. One factor that turns out to be important is the emissivity of the surface. A shiny metallic surface has low absorptivity (most of the heat re-

flects off) but also has low emissivity (does not radiate much heat away). A bright white surface also has low absorptivity, but has high emissivity (radiates a lot of heat away).

On a clear sunny day, the sun is a very bright heat source, but the sky away from the sun is at a very low radiation temperature. If you can arrange to reflect, or otherwise keep the sun's direct radiation away, you can achieve a fair amount of cooling by arranging for a high emissivity surface to radiate to the open sky.

Where Can You Find Us?

March '98

- American Institute of Chemical Engineers National Meeting, New Orleans: "Statistical DOE for Improvement of Fertilizer Products"
- American Chemical Society National Conference, Poster Session, Dallas (Booth 946): "Computer Aided DOE for Mixtures"

April '98

- 18th Quality Expo, Chicago (Booth 20059): "Real Life DOE"

May '98

- 51st Annual Quality Congress, Philadelphia (Booth 605): "Keys to Successful Designed Experiments"

August '98

- Joint Statistical Meetings, Dallas (Booth to be announced): "Teaching Aids for DOE" and "DOE on Paraffin Blend for Therapeutic Bath"

Invite us to your regional or national conference. Send e-mail to mark@statease.com

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The Prob>|t| values for the pure quadratic coefficients (A^2 and B^2) are not significant since they are greater than 0.10. However, let's leave these terms in the model and look at the 3D view of the

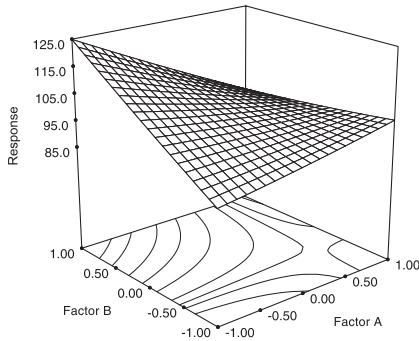


Figure 3: 3D Surface of Full Quadratic Fit

model graph (figure 3). Now delete the pure quadratic terms, A^2 and B^2 , leaving a factorial model:

Factor	Coefficient Estimate	t for H_0 Coeff=0	Prob> t
Intercept	99.77		
A-Factor A	-5.44	-14.12	<0.0001
B-Factor B	7.79	20.22	<0.0001
AB	-11.37	-24.11	<0.0001

Table 2: Reduced Model (Factorial)

The fit using the reduced (factorial) model is as good as with the full quadratic. Figure 4, the 3D surface for reduced quadratic, supports this statement. You can see that it is nearly identical to figure 3. However, you may be misled by changes in leverage. Because the ratio of coefficients to points decreases with model reduction, ALL the leverages are

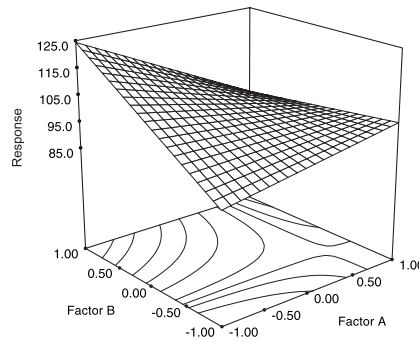


Figure 4: 3D Surface of Reduced Model (Factorial)

Table 3: Table of Leverages (# Flagged)

Std	Type	A	B	Response	Leverage	
					Full Model (Quadratic)	Reduced (Factorial)
1	Factorial	-1.0	-1.0	85.9	0.79	0.66 #
2	Factorial	+1.0	-1.0	98.8	0.79	0.66 #
3	Factorial	-1.0	+1.0	124.4	0.79	0.66 #
4	Factorial	+1.0	+1.0	91.9	0.79	0.66 #
5	Axial	-1.0	0.0	106.5	0.49	0.24
6	Axial	+1.0	0.0	93.4	0.49	0.24
7	Axial	0.0	-1.0	92.3	0.49	0.24
8	Axial	0.0	+1.0	107.5	0.49	0.24
9	Center	0.0	0.0	98.4	0.17	0.077
10	Center	0.0	0.0	99.0	0.17	0.077
11	Center	0.0	0.0	100.2	0.17	0.077
12	Center	0.0	0.0	99.1	0.17	0.077
13	Center	0.0	0.0	99.6	0.17	0.077
Average Leverage:					0.46	0.31

reduced, some more than others. The leverages of axial and center points are greatly reduced when the quadratic coefficients are eliminated (this is good!), but the leverages of the factorial points are hardly affected.

However, after model reduction, the factorial point leverages (std runs 1-4) are now greater than two times the average, so they get flagged. However, they are still less than for the previous full quadratic model. Therefore, in this case, they may be flagged, but they're not bad.

— Pat Whitcomb (e-mail: pat@statease.com)

Attention DOE Teachers at Universities and Colleges



A 180-day time-limited version of Design-Expert® software (CD-ROM) is now available for purchase through John Wiley & Sons Publishing. It is bundled along with Douglas Montgomery's *Design & Analysis of Experiments*, 4th Edition, for \$97.95. The CD includes "on-line" tutorials and Adobe's Acrobat Reader for PDR. The tutorials are keyed to Montgomery's book. It is also available separately for \$29.95. The contact person at John Wiley is Wayne Anderson at 212-850-6300.

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